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RESEARCH REPORT: RR 25810
(CSI # 03151)

BASED UPON ICC ES EVALUATION SERVICE
REPORT NO. ESR-2272

REEVALUATION DUE DATE:
August 1, 2010
Issued Date: August 1, 2009
Code: 2008 LABC

GENERAL APPROVAL – Powers Snake+ Anchors for Cracked and Uncracked Concrete

DETAILS

The above assemblies and/or products are approved when in compliance with the description, use, identification and findings of ICC Evaluation Services Report No. ESR-2272 dated September 1, 2008, revised June 2009, of the ICC Evaluation Service, Incorporated. The report in its entirety is attached and made part of this general approval.

The parts of Report No.ESR-2272 which are excluded on the attached copy have been removed by the Los Angeles Building as not being included in this approval.

The approval is subject to the following conditions:

1. The allowable and strength design values listed in the attached report and tables are for the fasteners only. Connected members shall be checked for capacity (which may govern).
2. The anchors shall be identified by labels on the packaging indicating the manufacturer's name and product designation.

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Powers Fasteners, Inc.

Re: Powers Snake+ Anchors for Cracked and Uncracked Concrete

3. The anchors shall be installed as per the attached manufacturer's instructions except as otherwise stated in this report. Copies of the installation instructions shall be available at each job site.
4. Design values and minimum embedment requirements shall be per Tables in ICC ES Report No. ESR-2272.
5. The concrete shall have attained its minimum design strength prior to installation of the anchors.
6. Special inspection in accordance with Section 91.1704 of the 2008 Los Angeles City Building Code shall be provided for anchor installations.
7. Anchors may be installed at embedment less than minimum depth per Table 1911.2 of the 2008 Los Angeles City Building Code for the following conditions:
 - a. Anchors are limited to the installation of Plumbing/fire sprinkler system, HVAC and electrical conduit.
 - b. 10 percent of the bolts are field load tested after installation. The bolt shall develop 300 percent of the allowable capacities listed in tables 5 through 13. If a failure occurs, then test 25% of the bolts.
8. The use of anchors is limited to dry interior locations.
9. The anchors are not approved for masonry application.
10. Calculations demonstrating that the applied loads or factored loads are less than the allowable load values or design strength level values respectively, described in this report shall be submitted to the plan check Engineer at the time of permit application. The calculations shall be prepared by a Civil or Structural Engineer registered in the State of California.

Powers Fasteners, Inc.

Re: Powers Snake+ Anchors for Cracked and Uncracked Concrete

DISCUSSION

The report is in compliance with 2008 Los Angeles Building Code.

The approval is based on tests in accordance with ICC ES Acceptance Criteria for Mechanical Anchors in Concrete Elements (AC 193), dated February 2009, which incorporate requirements in ACI 355.2-04, for use in cracked and uncracked concrete, and quality control documentation.

This general approval will remain effective provided the Evaluation Report is maintained valid and unrevised with the issuing organization. Any revision to the report must be submitted to this Department for review with appropriate fee to continue the approval of the revised report.

Addressee to whom this Research Report is issued is responsible for providing copies of it, complete with any attachments indicated, to architects, engineers and builders using items approved herein in design or construction which must be approved by Department of Building and Safety Engineers and Inspectors.

This general approval of an equivalent alternate to the Code is only valid where an engineer and/or inspector of this Department has determined that all conditions of this Approval have been met in the project in which it is to be used.

Powers Fasteners offers software to assist in the design of anchorages using Powers Fasteners products. The software "PDA Powers Design Assist" includes selectable Strength Design methodology utilizing ICC-ES AC193-compliant data to generate designs in conformance with the 2008 Los Angeles City Building Code. The PDA Software may be downloaded at www.Powers.com.

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Attachment: ICC ES Report No. ESR-2272 (9 Pages)

ICC-ES Evaluation Report

ESR-2272*

Issued September 1, 2008

This report is subject to re-examination in one year.

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A Subsidiary of the International Code Council®

DIVISION: 03—CONCRETE
Section: 03151—Concrete Anchoring
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EVALUATION SUBJECT:
POWERS SNAKE+ ANCHORS IN CRACKED AND UNCRACKED CONCRETE
1.0 EVALUATION SCOPE
Compliance with the following codes:

- 2006 *International Building Code*® (IBC)
- * ▪ ~~2006 *International Residential Code*® (IRC)~~
- ~~2003 *International Building Code*® (IBC)~~
- ~~2003 *International Residential Code*® (IRC)~~

Property evaluated:

Structural

2.0 USES

The Powers Snake+ anchor is used to resist static, wind and seismic tension and shear loads in cracked and uncracked structural normal-weight concrete and structural sand-lightweight concrete having a specified compressive strength, f'_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa); and in cracked and uncracked normal-weight or structural sand-lightweight concrete over steel deck having a minimum specified compressive strength, f'_c , of 3,000 psi (20.7 MPa). The anchoring system is an alternative to cast-in-place anchors described in Sections 1911 and 1912 of the 2006 IBC and 1912 and 1913 of the 2003 IBC. The anchors may also be used where an engineered design is submitted in accordance with Section R301.1.3 of the 2006 and 2003 IRC.

3.0 DESCRIPTION
3.1 Snake+ Anchors:

Snake+ anchors are one-piece, internally threaded screw anchors which receive threaded steel inserts. The anchors are manufactured from carbon steel, which are case hardened and have a minimum 0.0002-inch (5 μ m) zinc plating. The Snake+ anchor is illustrated in Figure 1. Installation information and dimensions are set forth in Section 4.3, Table 1 and Figure 3.

3.2 Steel Insert Elements:

Threaded steel insert elements must be threaded into the Snake+ Anchors to form a connection. The material properties of the steel insert elements must comply with Tables 2 and 3.

3.3 Concrete:

Normal-weight and structural sand-lightweight concrete must comply with Sections 1903 and 1905 of the IBC.

3.4 Steel Deck Panels:

Steel deck panels must comply to the requirements of ASTM A 653 and have a minimum base metal thickness of 0.035-inch (20 gage).

4.0 DESIGN AND INSTALLATION
4.1 Strength Design:

- 4.1.1 General:** Design strengths must be determined in accordance with ACI 318-05 (2006 IBC) Appendix D or ~~ACI 318-02 (2003 IBC) Appendix D~~, and this report. Design parameters are provided in Tables 2 and 3. Strength reduction factors, ϕ , as given in Tables 2 and 3 must be used for load combinations calculated in accordance with Section 1605.2.1 of the IBC or Section 9.2 of ACI 318.

4.1.2 Requirements for Static Steel Strength in Tension, N_{sa} : The nominal static steel strength, N_{sa} , of steel insert elements in tension must be calculated in accordance with ACI 318 D.5.1. The resulting values for a single anchor are described in Table 2 of this report.

4.1.3 Requirements for Static Concrete Breakout Strength of Anchor or Anchors in Tension N_{cb} or N_{cbg} : The nominal concrete breakout strength in tension, N_{cb} and N_{cbg} , respectively, must be calculated in accordance with ACI 318 D.5.2, with modifications as described in this section. The basic concrete breakout strength of a single anchor in tension must be calculated in accordance with ACI 318 D.5.2.2, using the values of h_{ef} where analysis indicates no cracking in accordance with ACI 318 D.5.2.6, the nominal concrete breakout strength in tension must be calculated with $\psi_{c,N} = 1.0$ and k_{uncl} as given in Table 2. For

*Revised June 2009

Snake+ anchors installed in the soffit of structural sand-lightweight or normal weight concrete on steel deck floor and roof assemblies, as shown in Figure 4, evaluation of concrete breakout capacity in accordance with ACI 318 D.5.2 is not required.

4.1.4 Requirements for Critical Edge Distance: For the Snake+ anchor, $C_{ac} = C_{a,min}$ with the value as given in Table 2. For the concrete breakout strength in tension for cracked and uncracked concrete, calculated according to ACI 318 D.5.2, the value $\psi_{ed,N} = 1.0$ for all cases.

4.1.5 Requirements for Static Pullout Strength of Anchor in Tension, N_{pn} : Where values for $N_{p,cr}$ or $N_{p,uncr}$ are not provided in Table 2, the pullout strength in tension in cracked and uncracked concrete need not be evaluated. The pullout strength in tension of the Snake+ anchor installed in the soffit of structural sand-lightweight or normal weight concrete on steel deck floor and roof assemblies, as shown in Figure 4, is provided in Table 2 of this report.

4.1.6 Requirements for Static Steel Shear Capacity, V_{sa} : In lieu of the values for nominal steel strength in shear, V_{sa} , as given in ACI 318 D.6.1.2 (c), the shear values given in Table 3 of this report must be used. The shear strength as governed by steel element failure of the Snake+ anchors installed in the soffit of structural sand-lightweight or normal weight concrete on steel deck floor and roof assemblies, $V_{sa,deck}$, as shown in Figure 4, is given in Table 3. The required steel insert strengths are presented in Table 3.

4.1.7 Requirements for Concrete Breakout Strength of Anchor or Anchors in Shear, V_{cb} or V_{cbg} : The nominal concrete breakout strength of a single anchor or group of anchors in shear, V_{cb} or V_{cbg} , respectively, must be calculated in accordance with ACI 318 D.6.2, with modifications as described in this section. The basic concrete breakout strength in shear, V_b , must be calculated in accordance with ACI 318 D.6.2 using the value of l_e and d_o provided in Table 3. The value of l_e used in ACI 318 Equation (D-24) is equal to h_{ef} .

For anchors installed in the soffit of structural sand-lightweight or normal-weight concrete-filled steel deck floor and roof assemblies, as shown in Figure 4, calculation of the concrete breakout strength in accordance with ACI 318 D.6.2 is not required.

4.1.8 Requirements for Concrete Pryout Strength of Anchor or Anchors in Shear, V_{cp} or V_{cpg} : The nominal concrete pryout strength of a single anchor or group of anchors, V_{cp} or V_{cpg} , respectively, must be calculated in accordance with ACI 318 D.6.3, modified by using the value of k_{cp} described in Table 3 of this report and the value of N_{cb} or N_{cbg} as calculated in Section 4.1.3 of this report.

For anchors installed in the soffit of structural sand-lightweight or normal-weight concrete-filled steel deck floor and roof assemblies, as shown in Figure 4, calculation of the concrete pryout strength in accordance with ACI 318 D.6.3 is not required.

4.1.9 Requirements for Minimum Member Thickness, Minimum Anchor Spacing and Minimum Edge Distance: In lieu of ACI 318 D.8.3, values of C_{min} and s_{min} as given in Table 1 of this report must be used. In lieu of ACI 318 D.8.5, minimum member thicknesses, h_{min} , as given in Table 1 of this report must be used.

For anchors installed through the soffit of steel deck assemblies, the anchors must be installed in accordance with Figure 4 of this report and must have an axial spacing along the flute equal to the greater of $3h_{ef}$ or 1.5 times the flute width.

4.1.10 Requirements for Seismic Design: For load combinations including seismic loads, the design must consider the additional requirements of ACI 318 D.3.3 as modified by Section 1908.1.16 of the 2006 IBC or the following:

Code	ACI 318 D.3.3 Seismic Region	Code Equivalent Design
2003-IBC and IRC	Moderate or high seismic risk	Seismic Design Categories C, D, E and F

The nominal steel strength and the nominal concrete breakout strength for anchors in tension, and the nominal concrete breakout strength for anchors in shear, must be calculated according to ACI 318 Sections D.5 and D.6, respectively, taking into account the corresponding values given in Tables 2 and 3.

The nominal pullout strength N_{eq} and nominal steel strength in shear V_{eq} must be evaluated with the values given in Table 2 and Table 3, respectively. Anchor steel must be classified as brittle in seismic tension calculations. Anchor steel may be classified as ductile for seismic shear calculations for the inserts recognized in this report. Applicable strength reduction factors, ϕ , are given in Table 2 and Table 3.

4.1.11 Interaction of Tensile and Shear Forces: Anchors or groups of anchors that are subject to the effects of combined axial (tensile) and shear, the design must be performed in accordance with ACI 318 D.7.

4.1.12 Structural Sand-Lightweight Concrete: When anchors are used in structural sand-lightweight concrete, N_b , N_{eq} , $N_{p,cr}$, $N_{p,uncr}$, V_b , V_{cp} and V_{cpg} must be multiplied by 0.60, in lieu of ACI 318 D.3.4.

For anchors installed in the soffit of structural sand-lightweight concrete-filled steel deck floor and roof assemblies, this reduction is not required.

4.2 Allowable Stress Design (ASD):

4.2.1 General: Design values for use with allowable stress design load combinations calculated in accordance with Section 1605.3 of the IBC must be established using the following equations:

$$T_{allowable,ASD} = \phi N_n / \alpha \tag{Eq-1}$$

$$V_{allowable,ASD} = \phi V_n / \alpha \tag{Eq-2}$$

where:

$$T_{allowable,ASD} = \text{Allowable tension load (lbf or kN)}$$

$$V_{allowable,ASD} = \text{Allowable shear load (lbf or kN)}$$

$$\phi N_n = \text{Lowest design strength of an anchor or anchor group in tension as determined in accordance with ACI 318 Appendix D, Section 4.1 of this report and 2006 IBC Section 1908.1.16, as appropriate (lbf or kN).}$$

$$\phi V_n = \text{Lowest design strength of an anchor or anchor group in shear as determined in accordance with ACI 318 Appendix D, Section 4.1 of this report and 2006 IBC Section 1908.1.16, as appropriate (lbf or kN).}$$

$$\alpha = \text{Conversion factor calculated as a weighted average of the load factors for the controlling load combination. In addition, } \alpha \text{ must include all applicable factors to account for nonductile failure modes and required over-strength.}$$

Limits on edge distance, anchor spacing and member thickness as given in Table 1 of this report must apply. An example of Allowable Stress Design tension values is given in Table 4 of this report.

4.2.2 Interaction of Tensile and Shear Forces: The interaction must be calculated and consistent with ACI 318 D.7, as follows:

For shear loads $V \leq 0.2V_{allowable,ASD}$, the full allowable load in tension $T_{allowable,ASD}$ must be permitted.

For tension loads $T \leq 0.2T_{allowable,ASD}$, the full allowable load in shear $V_{allowable,ASD}$ must be permitted.

For all other cases:
$$\frac{T}{T_{allowable,ASD}} + \frac{V}{V_{allowable,ASD}} \leq 1.2 \quad (\text{Eq-3})$$

4.3 Installation:

Installation parameters are provided in Table 1, and Figures 2, 3 and 4. The Snake+ anchor must be installed according to manufacturer's published installation instructions and this report. Anchors must be installed in holes drilled into concrete using carbide-tipped masonry drill bits complying with ANSI B212.15-1994. The drill bit size and drilled hole depth must be in accordance with Table 1. The anchors must be installed in drilled holes with a powered impact screwdriver and fitted with a Snake+ setting tool supplied by Powers Fasteners. The allowable ranges of installation parameters for the Snake+ anchors using powered impact screwdriver are given in Table 1. The anchors must be driven until the shoulder of the Snake+ setting tool comes into contact with the surface of the concrete. The minimum thread engagement of a threaded rod or bolt insert element assembly into the Snake+ anchor must be full anchor depth.

4.4 Special Inspection:

Special inspection is required in accordance with Section 1704.13 of the IBC and, as applicable, Section 1701.5.2 of the UBC. The special inspector must make periodic inspections during anchor installation to verify anchor type, anchor dimensions, concrete type, concrete compressive strength, hole dimensions, steel insert element type and dimensions, anchor spacing, edge distances, concrete thickness, anchor embedment, steel insert element depth, maximum tightening torque and adherence to the manufacturer's printed installation instructions. The special inspector must be present as often as required in accordance with the "statement of special inspection." Under the IBC, additional requirements as set forth in Sections 1705 and 1706 must be observed, where applicable.

5.0 CONDITIONS OF USE

The Powers Snake+ anchors described in this report comply with, or are suitable alternatives to what is specified in, those codes indicated in Section 1.0 of this report, subject to the following conditions:

- 5.1 Anchor and steel insert element sizes, dimensions, and minimum embedment depth are as set forth in this report.
- 5.2 The anchors and inserts must be installed in accordance with the manufacturer's published installation instructions and this report. In case of conflict, this report governs.
- 5.3 Anchors must be limited to use in cracked and uncracked normal weight concrete and structural sand-lightweight concrete having a specified compressive strength, f'_c , of 2,500 psi to 8,500 psi (17.2 MPa to 58.6 MPa), and cracked and uncracked

normal weight or structural sand-lightweight concrete over steel deck having a minimum specified compressive strength, f'_c , of 3,000 psi (20.7 MPa).

- 5.4 The values of f'_c used for calculation purposes must not exceed 8,000 psi (55.1 MPa).
- 5.5 Strength design values must be established in accordance with Section 4.1 of this report.
- 5.6 Allowable stress design values must be established in accordance with Section 4.2 of this report.
- 5.7 Anchor spacing and edge distance, as well as minimum member thickness, must comply with Table 1 of this report.
- 5.8 Prior to installation, calculations justifying that the design loads comply with this report must be submitted to the code official for approval. The calculations and details must be prepared by a registered design professional where required by the statutes of the jurisdiction in which the project is to be constructed.
- 5.9 Since an ICC-ES acceptance criteria for evaluating data to determine the performance of screw anchors subjected to fatigue or shock loading is unavailable at this time, the use of these anchors under such conditions is beyond the scope of this report.
- 5.10 Anchors may be installed in regions of concrete where cracking under service load conditions has occurred or where analysis indicates cracking may occur ($f_t > f_r$), subject to the conditions of this report.
- 5.11 Anchors may be used to resist short-term loading due to wind or seismic forces in locations designated as Seismic Design Categories A through F, subject to the conditions of this report.
- 5.12 Anchors are not permitted to support fire-resistance-rated construction. Where not otherwise prohibited by the code, anchors are permitted for installation in fire-resistance-rated construction provided that at least one of the following conditions is fulfilled:
 - Anchors are used to resist wind or seismic forces only.
 - Anchors that support gravity load-bearing structural elements are within a fire-resistance-rated envelope or a fire-resistance-rated membrane, are protected by approved fire-resistance-rated materials, or have been evaluated for resistance to fire exposure in accordance with recognized standards.
 - Anchors are used to support nonstructural elements.
- 5.13 Snake+ anchors must not be removed from concrete and reused.
- 5.14 Anchors have been evaluated for reliability against brittle failure and found to be not significantly sensitive to brittle failure such as hydrogen embrittlement.
- 5.15 Special inspection must be provided in accordance with Section 4.4 of this report.
- 5.16 Use of anchors is limited to dry, interior locations.
- 5.17 Anchors are manufactured under an approved quality control program with inspections by CEL Consulting (AA-639).

6.0 EVIDENCE SUBMITTED

Data in accordance with the ICC-ES Acceptance Criteria for Mechanical Anchors in Concrete Elements (AC193), which incorporates requirements in ACI 355.2-04, dated February 2009, for use in cracked and uncracked concrete and quality control documentation.

7.0 IDENTIFICATION

The Snake+ anchors are identified by their dimensional characteristics and anchor size. Packages are identified with the anchor name, type and size, the company name

as set forth in Table A of this report, and the name of the quality control agency (CEL), and evaluation report number (ESR-2272).

TABLE A—PRODUCT NAMES BY COMPANY

COMPANY NAME	PRODUCT NAME
Powers Fasteners, Inc.	Wedge-Bolt+
L. H. Dottie Co.	Dottie Snake+



FIGURE 1—SNAKE+ SCREW ANCHOR AND SETTING TOOL

TABLE 1—INSTALLATION INFORMATION FOR SNAKE+ SCREW ANCHOR

Anchor Property / Setting Information	Notation	Units	Nominal Anchor Size
			³ / ₈ inch
Nominal outside anchor diameter	d_o	in. (mm)	¹ / ₂ (12.7)
Internal thread diameter (UNC)	d	in. (mm)	0.375 (9.5)
Nominal drill bit diameter	d_{bit}	in.	¹ / ₂ ANSI
Nominal embedment depth	h_{nom}	in. (mm)	1- ⁵ / ₈ (41)
Effective embedment	h_{ef}	in. (mm)	1.10 (28)
Minimum hole depth	h_o	in. (mm)	2 (51)
Minimum concrete member thickness ¹	h_{min}	in. (mm)	4 (102)
Overall anchor length	l_{anch}	in. (mm)	1- ¹ / ₄ (32)
Minimum edge distance ¹	c_{min}	in. mm	3 (76)
Minimum spacing distance ¹	s_{min}	in. mm	3 (76)
Critical edge distance ¹	c_{ac}	in. (mm)	3 (76)
Maximum impact screwdriver power (torque)	T_{screw}	ft.-lb. (N-m)	345 (468)
Minimum diameter of hole clearance in fixture for steel insert element (following anchor installation)	d_h	in (mm)	⁷ / ₁₆ (11)
Maximum tightening torque of steel insert element (threaded rod or bolt)	T_{max}	ft.-lb. (N-m)	8 (11)

¹For installations into the soffit of concrete over steel deck floor and roof assemblies, see Figure 4. Anchors in the lower flute may be installed with a maximum 1-inch (25.4 mm) offset in either direction. In addition, anchors must have an axial spacing along the flute equal to or greater of $3h_{ef}$ or 1.5 times the flute width.

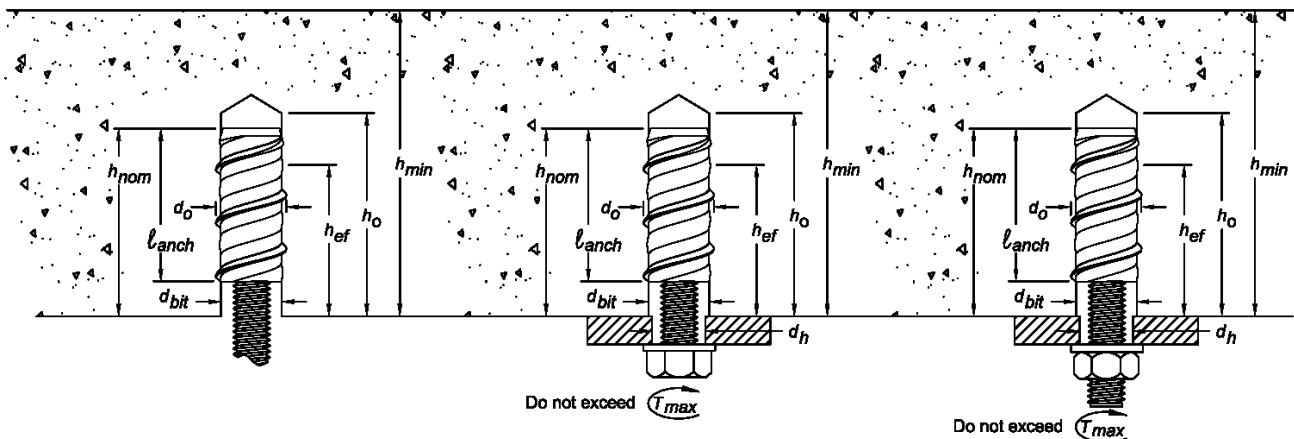


FIGURE 2—SNAKE+ SCREW ANCHOR INSTALLED WITH STEEL INSERT ELEMENT

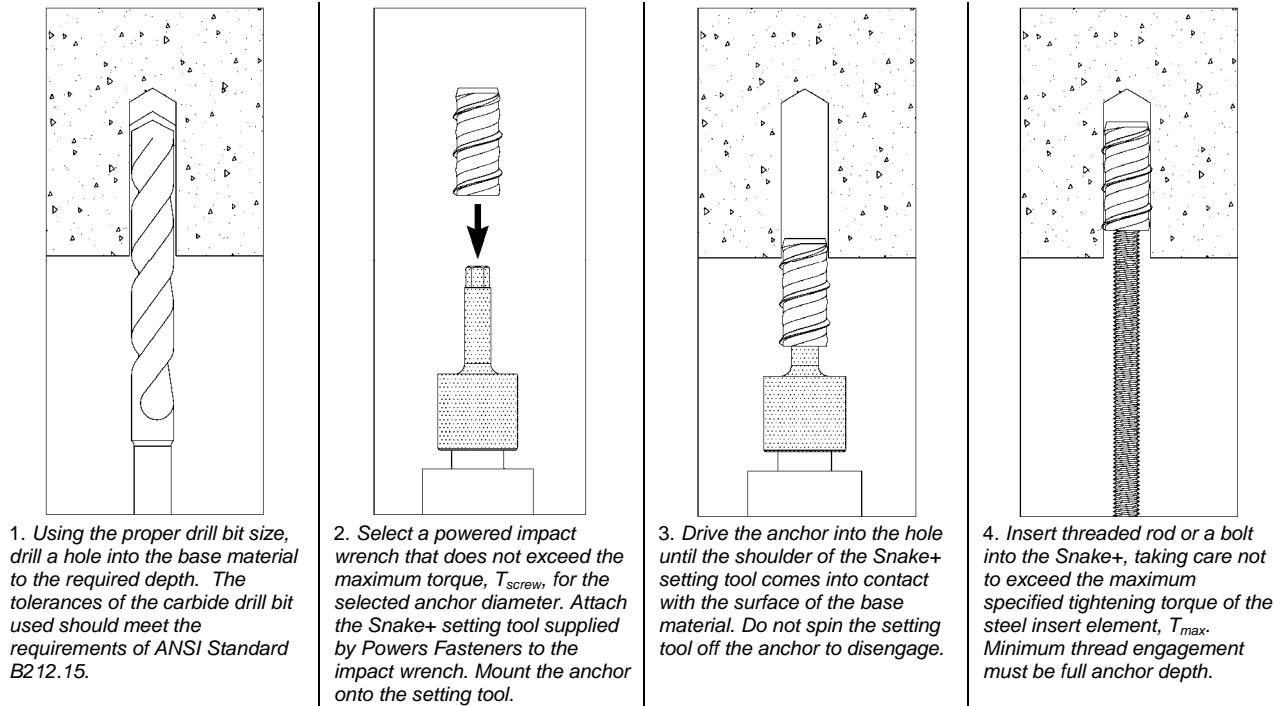


FIGURE 3—SNAKE+ SCREW ANCHOR INSTALLATION INSTRUCTIONS

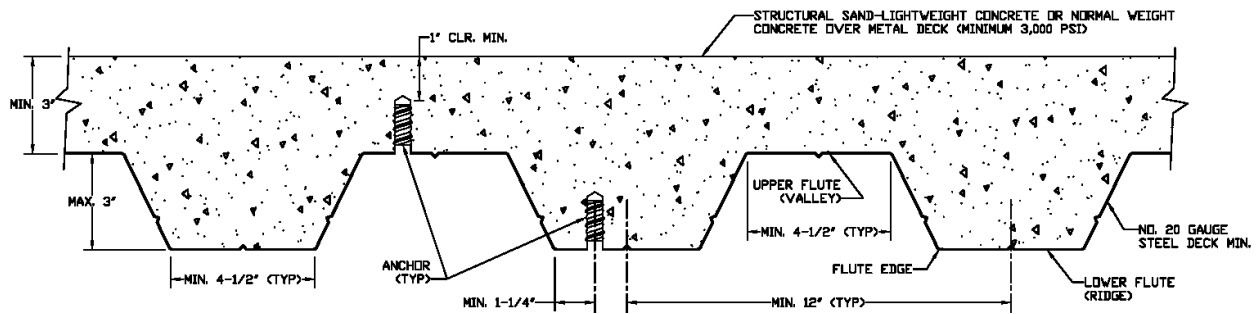


FIGURE 4—SNAKE+ SCREW ANCHOR INSTALLATION IN THE SOFFIT OF CONCRETE OVER STEEL DECK FLOOR AND ROOF ASSEMBLIES

TABLE 2—TENSION DESIGN INFORMATION FOR SNAKE+ SCREW ANCHORS IN CONCRETE
(For use with load combinations taken from ACI 318 Section 9.2)^{1,2}

Design Characteristic	Notation	Units	Nominal Anchor Size	
			3/8"	
Anchor category	1, 2 or 3	-	1	
Nominal embedment depth	h_{nom}	in.	1-5/8	
STEEL STRENGTH IN TENSION⁴				
Minimum specified yield strength of steel insert element (threaded rod or bolt)	f_y	ksi (N/mm ²)	SAE J429, Grade 2 or ASTM A 307, Grade C	36.0 (248)
		ksi (N/mm ²)	ASTM A193, Grade B7	105.0 (724)
Minimum specified ultimate strength of steel insert element (threaded rod or bolt)	f_{uta}^{10}	ksi (N/mm ²)	SAE J429, Grade 2 or ASTM A 307, Grade C	58.0 (400)
		ksi (N/mm ²)	ASTM A193, Grade B7	125.0 (862)
Effective tensile stress area of steel insert element (threaded rod or bolt)	A_{se}	in ² (mm ²)	0.0775 (50)	
Steel insert strength in tension	N_{sa}^{10}	lb (kN)	SAE J429, Grade 2 or ASTM A 307, Grade C	4,495 (20.0)
		lb (kN)	ASTM A193, Grade B7	9,685 (43.1)
Reduction factor for steel strength ³	ϕ	-	0.65	
CONCRETE BREAKOUT STRENGTH IN TENSION⁸				
Effective embedment	h_{ef}	in. (mm)	1.10 (28)	
Effectiveness factor for uncracked concrete	k_{uncr}	-	24	
Effectiveness factor for cracked concrete	k_{cr}	-	17	
Modification factor for cracked and uncracked concrete	$\psi_{c,N}^{10}$	-	1.0 See note 5	
Critical edge distance	c_{ac}	in. (mm)	3 (76)	
Reduction factor for concrete breakout strength ³	ϕ	-	0.65 (Condition B)	
PULLOUT STRENGTH IN TENSION (NON-SEISMIC APPLICATIONS)⁸				
Characteristic pullout strength, uncracked concrete (2,500 psi)	$N_{p,uncr}$	lb (kN)	See note 7	
Characteristic pullout strength, cracked concrete (2,500 psi)	$N_{p,cr}$	lb (kN)	See note 7	
Reduction factor for pullout strength ³	ϕ	-	0.65 (Condition B)	
PULLOUT STRENGTH IN TENSION FOR SEISMIC APPLICATIONS⁸				
Characteristic pullout strength, seismic (2,500 psi)	N_{eq}^{10}	lb (kN)	See note 7	
Reduction factor for pullout strength ³	ϕ	-	0.65 (Condition B)	
PULLOUT STRENGTH IN TENSION FOR STRUCTURAL SAND-LIGHTWEIGHT AND NORMAL-WEIGHT CONCRETE OVER STEEL DECK				
Characteristic pullout strength, uncracked concrete over steel deck ^{6,9}	$N_{p,deck,uncr}$	lb (kN)	1,515 (6.7)	
Characteristic pullout strength, cracked concrete over steel deck ^{6,9}	$N_{p,deck,cr}$	lb (kN)	1,075 (4.8)	
Reduction factor for pullout strength ³	ϕ	-	0.65 (Condition B)	

¹The data in this table is intended to be used with the design provisions of ACI 318 Appendix D; for anchors resisting seismic loads the additional requirements of ACI 318 D.3.3 shall apply.

²Installation must comply with published instructions and details and information in this report.

³All values of ϕ were determined from the load combinations of ACI 318 Section 9.2 and IBC Section 1605.2 and Condition B in accordance with ACI 318 D.4.4. If the load combinations of ACI 318 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318 D.4.5.

⁴It is assumed that the threaded rod or bolt used with the Snake+ screw anchor will be a ductile steel element as defined by ACI 318 D.1.

⁵For all design cases use $\psi_{c,N} = 1.0$. The appropriate effectiveness factor for cracked concrete (k_{cr}) or uncracked concrete (k_{uncr}) must be selected.

⁶For concrete compressive strength greater than 3,000 psi, $N_{pn} = (\text{Pullout strength value from table}) \times (\text{specified concrete compressive strength}/3000)^{0.5}$

⁷Pullout strength does not control design of indicated anchors and does not need to be calculated.

⁸Anchors are permitted to be used in structural sand-lightweight concrete provided that N_b , N_{eq} and N_{pn} are multiplied by a factor of 0.60.

⁹Values for $N_{p,deck}$ are for structural sand-lightweight concrete ($f'_{c,min} = 3,000$ psi) and additional lightweight concrete reduction factors need not be applied. In addition, evaluation for the concrete breakout capacity in accordance with ACI 318 D.5.2 is not required for anchors installed in the flute (soffit).

* ¹⁰For 2003 IBC code basis replace f_{uta} with f_{ut} ; N_{sa} with N_s ; $\psi_{c,N}$ with ψ_s and N_{eq} with $N_{p,seis}$

TABLE 3—SHEAR DESIGN INFORMATION FOR SNAKE+ SCREW ANCHORS IN CONCRETE
(For use with load combinations taken from ACI 318 Section 9.2)^{1,2}

Design Characteristic	Notation	Units	Nominal Anchor Size	
			³ / ₈ "	
Anchor category	1, 2 or 3	-	1	
Nominal embedment depth	h_{nom}	in.	1- ⁵ / ₈	
STEEL STRENGTH IN SHEAR⁴				
Minimum specified yield strength of steel insert element (threaded rod or bolt)	f_y	ksi (N/mm ²)	SAE J429, Grade 2 or ASTM A 307, Grade C	36.0 (248)
		ksi (N/mm ²)	ASTM A193, Grade B7	105.0 (724)
Minimum specified ultimate strength of steel insert element (threaded rod or bolt)	f_{uta} ⁸	ksi (N/mm ²)	SAE J429, Grade 2 or ASTM A 307, Grade C	58.0 (400)
		ksi (N/mm ²)	ASTM A193, Grade B7	125.0 (862)
Effective shear stress area of steel insert element (threaded rod or bolt)	A_{se}	in ² (mm ²)	0.0775 (50)	
Steel insert strength in shear	V_{sa} ⁸	lb (kN)	SAE J429, Grade 2 or ASTM A 307, Grade C	770 (3.4)
		lb (kN)	ASTM A193, Grade B7	1,655 (7.3)
Reduction factor for steel strength ³	ϕ	-	0.65	
CONCRETE BREAKOUT STRENGTH IN SHEAR⁵				
Load bearing length of anchor (h_{ef} or $8d_o$, whichever is less)	ℓ_e ⁸	in. (mm)	1.10 (28)	
Nominal anchor diameter	d_o	in. (mm)	0.375 (9.5)	
Reduction factor for concrete breakout strength ³	ϕ	-	0.70 (Condition B)	
CONCRETE PRYOUT STRENGTH IN SHEAR⁵				
Coefficient for prout strength (1.0 for $h_{ef} < 2.5$ in., 2.0 for $h_{ef} \geq 2.5$ in.)	k_{cp}	-	1.0	
Effective embedment	h_{ef}	in. (mm)	1.10 (28)	
Reduction factor for prout strength ³	ϕ	-	0.70 (Condition B)	
STEEL STRENGTH IN SHEAR FOR SEISMIC APPLICATIONS				
Steel insert strength in shear, seismic	V_{eq} ⁸	lb (kN)	SAE J429, Grade 2 or ASTM A 307, Grade C	770 (3.4)
		lb (kN)	ASTM A193, Grade B7	1,655 (7.4)
Reduction factor for steel strength in shear for seismic applications ³	ϕ	-	0.65	
STEEL STRENGTH IN SHEAR FOR STRUCTURAL SAND-LIGHTWEIGHT AND NORMAL-WEIGHT CONCRETE OVER STEEL DECK⁷				
Steel strength in shear, concrete over steel deck ⁶	$V_{sa,deck}$	lb (kN)	SAE J429, Grade 2 or ASTM A 307, Grade C	770 (3.4)
		lb (kN)	ASTM A193, Grade B7	1,655 (7.4)
Reduction factor for steel strength in shear for steel deck applications ³	ϕ	-	0.65	

¹The data in this table is intended to be used with the design provisions of ACI 318 Appendix D; for anchors resisting seismic loads the additional requirements of ACI 318 D.3.3 shall apply.

²Installation must comply with published instructions and details and information in this report.

³All values of ϕ were determined from the load combinations of ACI 318 Section 9.2, Condition B in accordance with ACI 318 D.4.4 and IBC Section 1605.2. If the load combinations of ACI 318 Appendix C are used, the appropriate value of ϕ must be determined in accordance with ACI 318 D.4.5.

⁴It is assumed that the threaded rod or bolt used with the Snake+ anchor will be a ductile steel element as defined by ACI 318 D.1.

⁵Anchors are permitted to be used in structural sand-lightweight concrete provided that N_p and N_{pn} are multiplied by a factor of 0.60.

⁶Values for $V_{sa,deck}$ are for structural sand-lightweight concrete ($f'_{c,min} = 3,000$ psi) and additional lightweight concrete reduction factors need not be applied. In addition, evaluation for the concrete breakout capacity in accordance with ACI 318 D.6.2 and the prout capacity in accordance with ACI 318 D.6.3 are not required for anchors installed in the flute (soffit).

⁷Shear loads for anchors installed through steel deck into concrete may be applied in any direction.

⁸For 2003 IBC code basis replace f_{uta} with f_{ut} ; V_{sa} with V_s ; and ℓ_e with ℓ and V_{eq} with $V_{sa,seis}$.

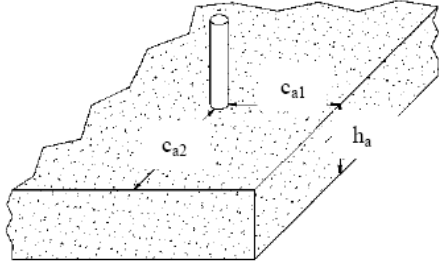
<p>GIVEN:</p> <ol style="list-style-type: none"> 1. Single 3/8-inch Snake+ anchor loaded in static tension only 2. Anchor used with ASTM A307, Grade C bolt ($f_{uts} = 58,000$ psi) 3. Concrete determined to remain uncracked for the life of the anchorage 4. No supplementary reinforcing present (assume Condition B) 5. $f'_c = 2,500$ psi (normal-weight concrete) 6. $c_{a1} = c_{a2} \geq c_{ac}$ 7. $h_a \geq h_{min}$ 8. Load combinations from ACI 318 Section 9.2 (no seismic loading) 9. 30% dead load and 70% live load, controlling load combination $1.2D + 1.6L$ 				
<p>Calculate the factored resistance strength, ϕN_n, and the allowable stress design value, $T_{allowable,ASD}$, for the given conditions.</p>				
<p>Calculation in accordance with ACI 318-05 Appendix D and this report:</p>				
<p>Step 1. Calculate steel strength of a single anchor in tension:</p> $\phi N_{sa} = \phi A_{se} f_{uta}$ $\phi N_{sa} = (0.65)(0.0775)(58,000) = 2,922 \text{ lbs.}$	D.5.1.2	Table 2		
<p>Step 2. Calculate concrete breakout strength of a single anchor in tension:</p> $\phi N_{cb} = \phi \frac{A_{Nc}}{A_{Nc0}} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b$ $N_b = k_c \sqrt{f'_c} h_{ef}^{1.5}$ $N_b = (24) \sqrt{2,500} (1.10)^{1.5} = 1,384 \text{ lbs.}$ $\phi N_{cb} = (0.65) \frac{(10.89)}{(10.89)} (1.0)(1.0)(1.0)(1,384) = 900 \text{ lbs.}$	D.5.2.1	Table 2		
<p>Step 3. Calculate pullout strength:</p> $\phi N_{pn} = \phi N_p \psi_{c,p}$ <p>$\phi N_{pn} = n/a$ (pullout strength does not control, see Table 2, footnote 7)</p>	D.5.3.2	Table 2		
<p>Step 4. Determine controlling resistance strength in tension:</p> $\phi N_n = \min[\phi N_{sa}, \phi N_{cb}, \phi N_{pn}] = \phi N_{cb} = 900 \text{ lbs.}$	D.4.1.1			
<p>Step 5. Calculate allowable stress design conversion factor for loading condition:</p> <p>Controlling load combination: $1.2D + 1.6L$</p> $\alpha = 1.2(30\%) + 1.6(70\%) = 1.48$	9.2			
<p>Step 6. Calculate allowable stress design value</p> $T_{allowable,ASD} = \frac{\phi N_n}{\alpha}$ $T_{allowable,ASD} = \frac{900}{1.48} = 608 \text{ lbs.}$		Sec. 4.2		

FIGURE 5—EXAMPLE OF FACTORED RESISTANCE STRENGTH AND CONVERSION TO ALLOWABLE STRESS DESIGN VALUE FOR ILLUSTRATIVE PURPOSES

ICC-ES Evaluation Report**ESR-2272 Supplement**

Issued June 1, 2009

This report is subject to re-examination on September 1, 2009.www.icc-es.org | (800) 423-6587 | (562) 699-0543 A Subsidiary of the International Code Council®**DIVISION: 03—CONCRETE**
Section: 03151—Concrete Anchoring**REPORT HOLDER:****POWERS FASTENERS, INC.**
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lane@lhdottie.com**EVALUATION SUBJECT:****POWERS SNAKE+ ANCHORS IN CRACKED AND UNCRACKED CONCRETE****1.0 EVALUATION SCOPE****Compliance with the following codes:**

- 2007 *Florida Building Code—Building*
- 2007 *Florida Building Code—Residential*

Property Evaluated:

Structural

2.0 PURPOSE OF THIS SUPPLEMENT

This supplement is issued to indicate that the Powers Snake+ Anchors in Cracked and Uncracked Concrete described in Sections 2.0 through 7.0 of the master report comply with the 2007 *Florida Building Code—Building* and the 2007 *Florida Building Code—Residential*, when designed and installed in accordance with the master evaluation report.

Use of the Powers Snake+ Anchors in Cracked and Uncracked Concrete as described in the master evaluation report for compliance with the High-Velocity Hurricane Zone provisions of the 2007 *Florida Building Code—Building* has not been evaluated, and is outside the scope of this supplement.

For products falling under Florida Rule 9B-72, verification that the report holder's quality assurance program is audited by a quality assurance entity approved by the Florida Building Commission for the type of inspections being conducted is the responsibility of an approved validation entity (or the code official when the report holder does not possess an approval by the Commission).

This supplement expires concurrently with the master report issued September 1, 2008.